



THE OHIO STATE UNIVERSITY

A Multi-Stepped Ultrasonic Horn for Industrial Scale Processes

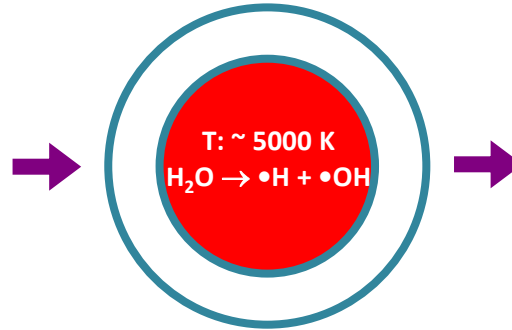
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Ruiyang Xiao, Gim-Yang Pee, Meiqiang Cai, Linda K Weavers

April 20th, 2015
Washington D.C.

Sonochemistry in Remediation

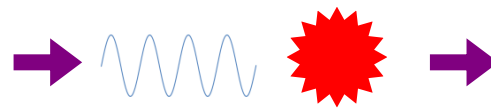


Cavitation



Transient cavitation bubble

- Oxidation
- Thermolysis



Micro-jet , micro-streaming
pitting, collision

- Desorption
- Accessibility

Scale Up Sonochemical Treatment

- Increase bioavailability, initiate degradation reaction, and enhance reaction rate
- Improve heat and mass transfer
- Designs in both ultrasonic devices and sono-reactors



Typical Ultrasonic Horn

- Shrinking dimension
- Small energy-emitting surface
- Concentrated cavitation volume
- Reduced contaminant removal



- **Low energy efficiency (13.3-28.1%)**
- **Scaling-up is very difficult!**



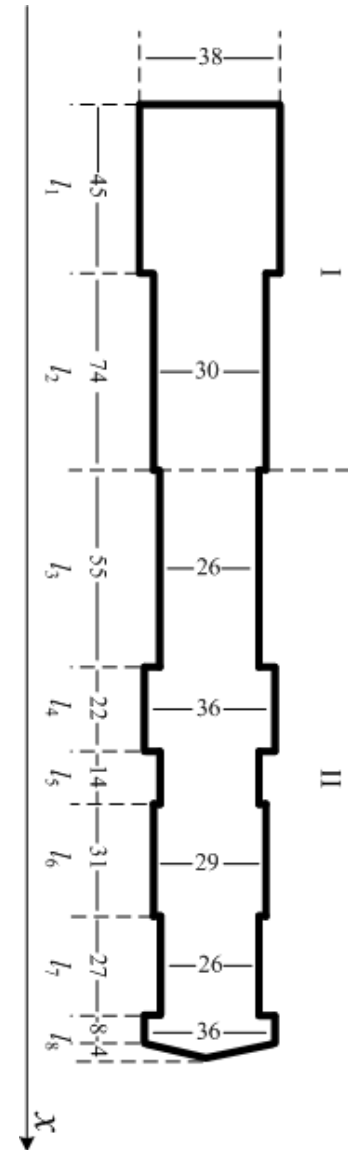
Objectives

- To design an improved horn configuration
- To characterize the designed horn
 - physical methods
 - chemical methods
- To evaluate large-scale application
 - hydrophone mapping
 - optimal size of sono-reactor

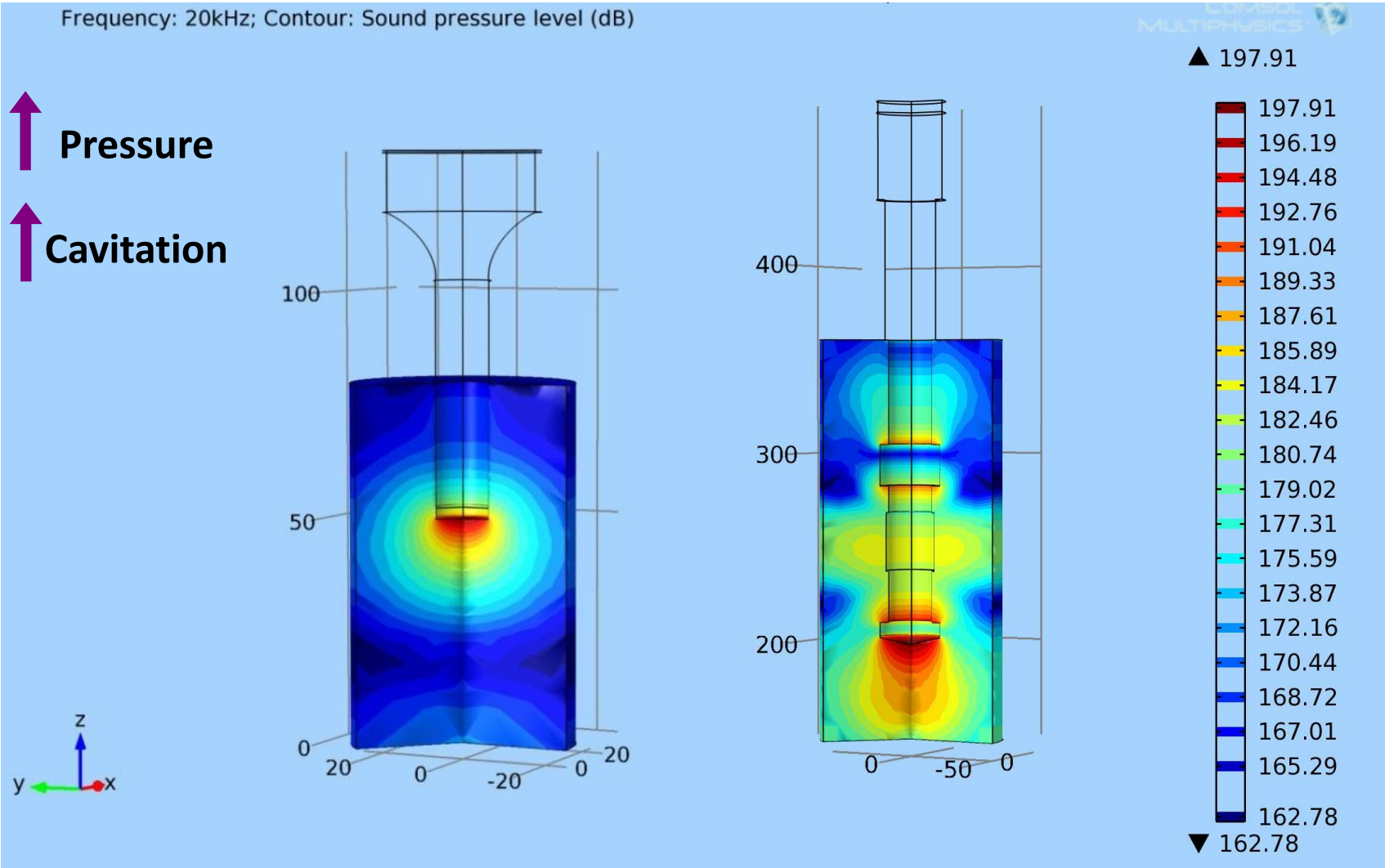


Design Steps

1. General requirements
 - resonance
2. Specific requirements
 - shape
3. Design principles
 - dynamic wave equation
 - equivalent circuit model
4. Verification using simulation
 - finite element analysis (FEA)
 - COMSOL Multiphysics



COMSOL Simulation



Typical horn

Designed horn

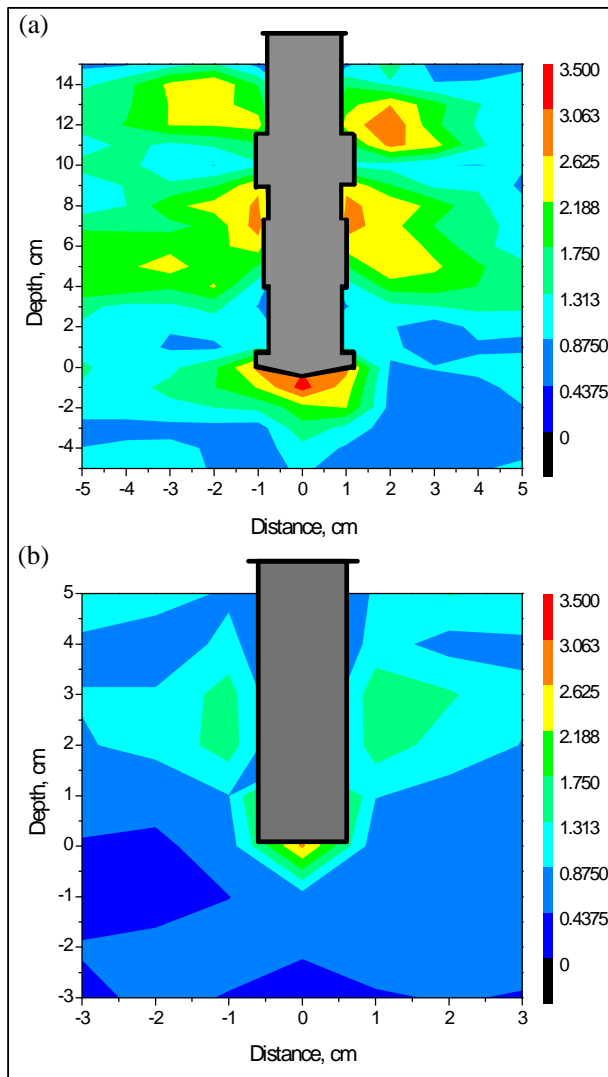
Horn Characterization



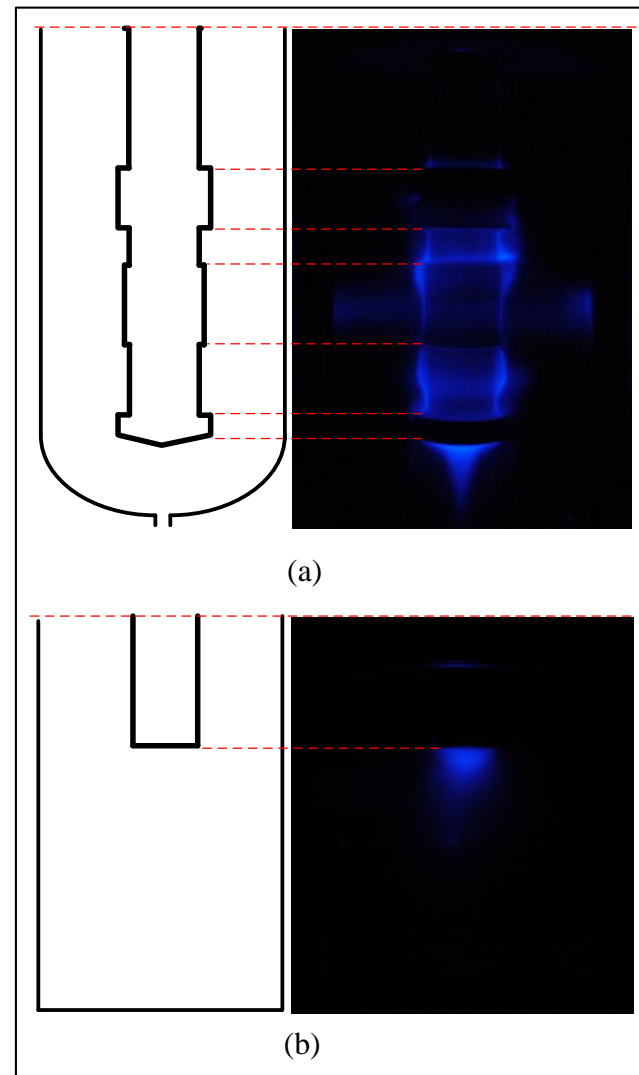
Designed horn



Typical horn





Hydrophone Measurements



Sonochemiluminescence (SCL)

Comparison - Energy, Cavitation, and Degradation

Horn	Energy efficiency (%)	^a Zero-order •OH formation rate constant ($\mu\text{M}/\text{min}$)	^b First-order degradation rate constants (1/min)
	31.5	0.36	0.022
	13.3	0.09	0.012

^a Initial concentration of terephthalate acid = 2mM; ^b initial concentration of phenanthrene = 10 μM



Energy Cost Estimation

Horn type	Typical	Designed
k, min^{-1}	0.0158	0.0217
t_{90}, min	145.5	106.1
P_{elec}, kW	0.275	1.000
V, L	0.04	1.25
$C_0, \mu\text{M}$	10.0	10.0
EE/O	1.67×10^4	1.41×10^3
Electricity price, \$ kWh ⁻¹	0.08	0.08
Cost, \$ per 1000L	1,330	113

8.5%

- Phenanthrene (first-order degradation)
- 90% removal
- \$0.08/kWh

$$EE/O = \frac{P_{elec} \times t_{90} \times 1000}{V \times 60 \times \log(C_0/C)}$$

Large-Scale Reactor Design

- Water tank setup

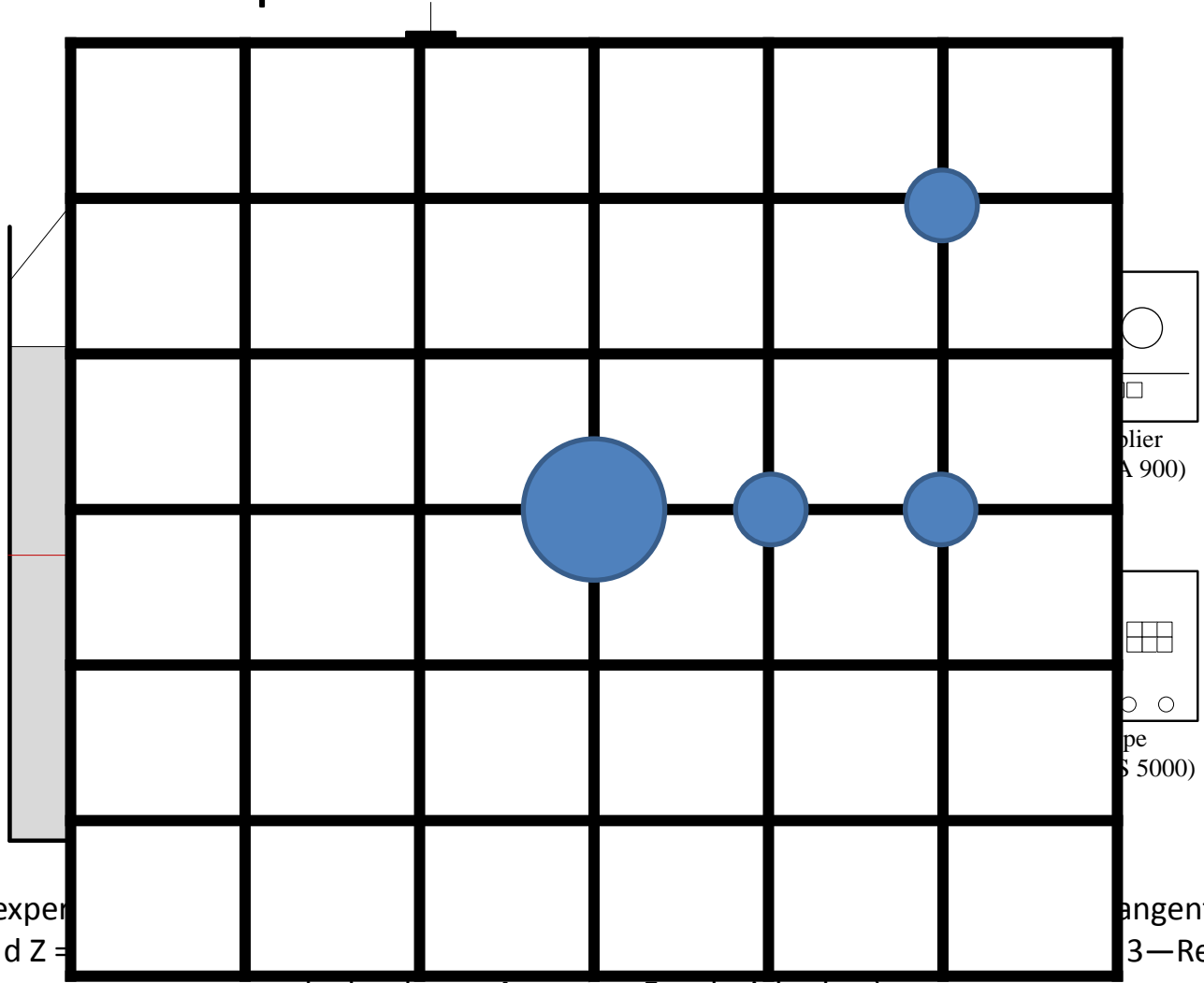


Diagram of exper
tip is define d Z =

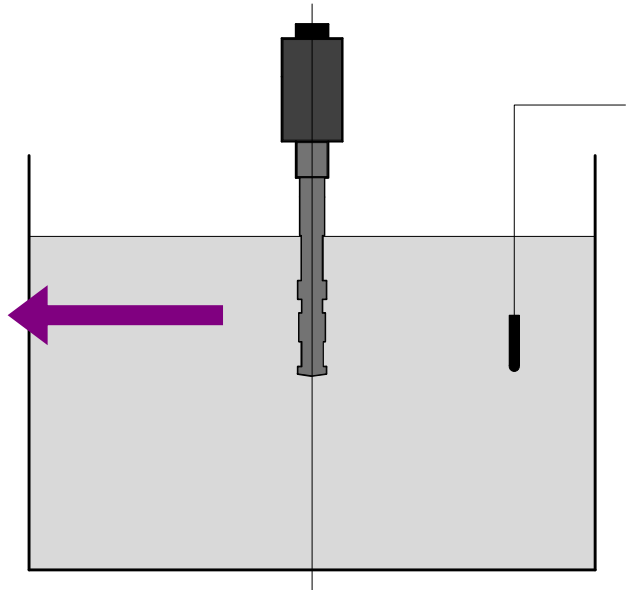
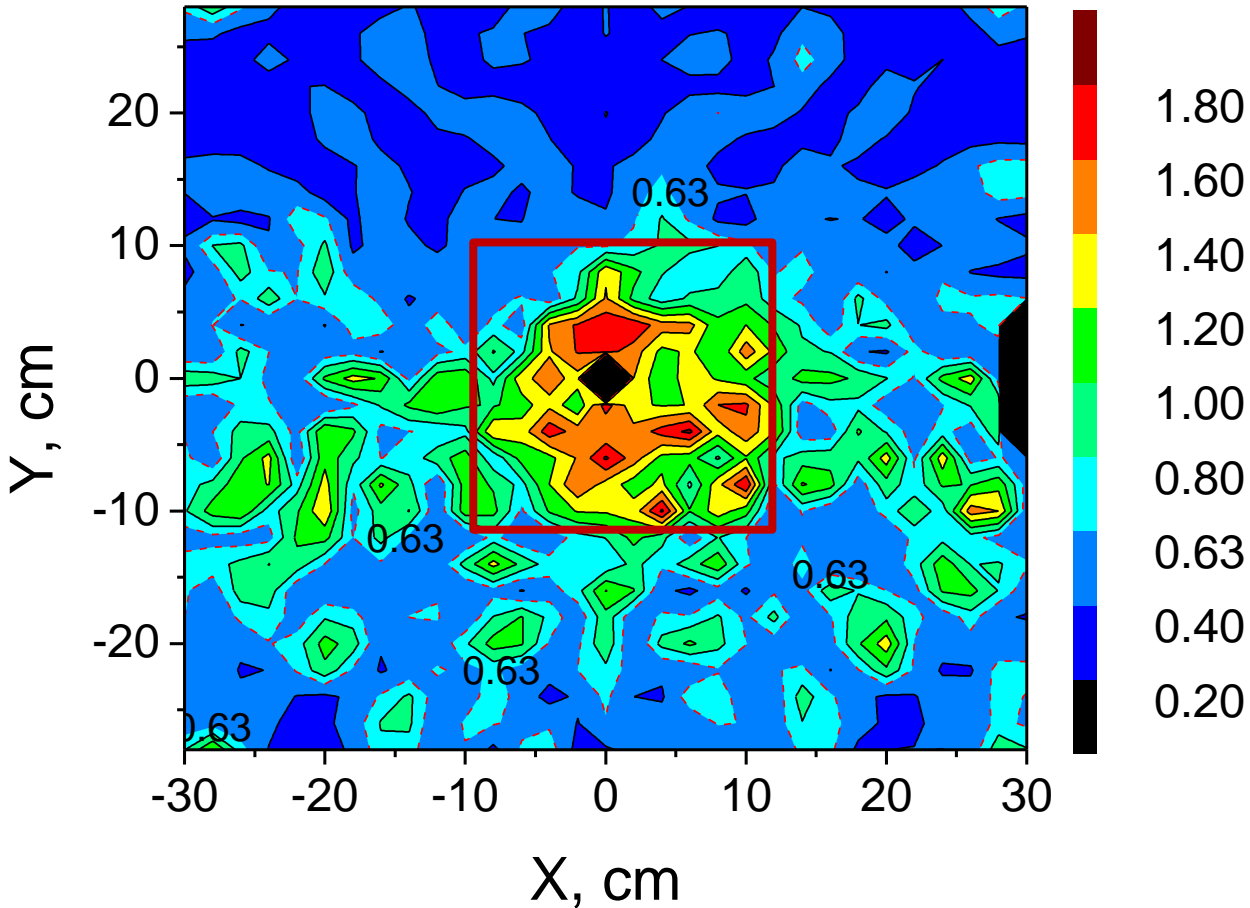
hydrophone; 4—water; 5—plexiglas box)

tangential to horn
3—Reson T4013



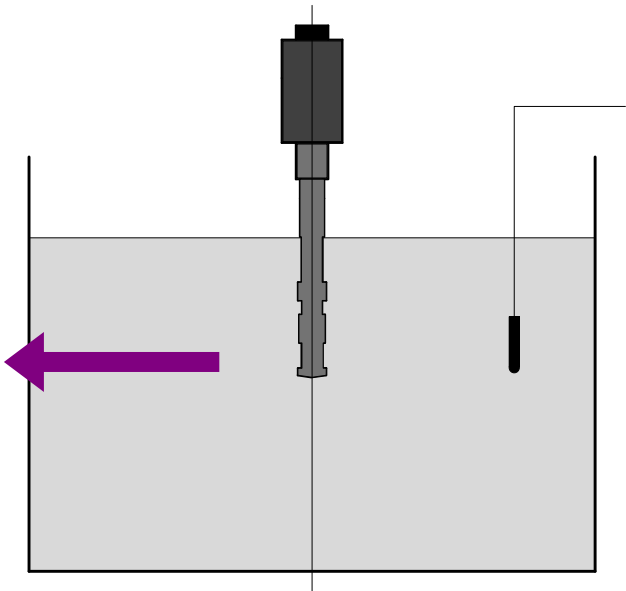
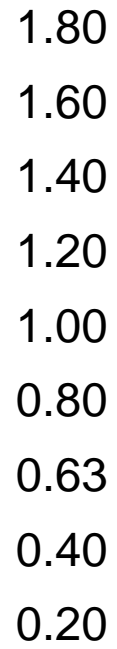
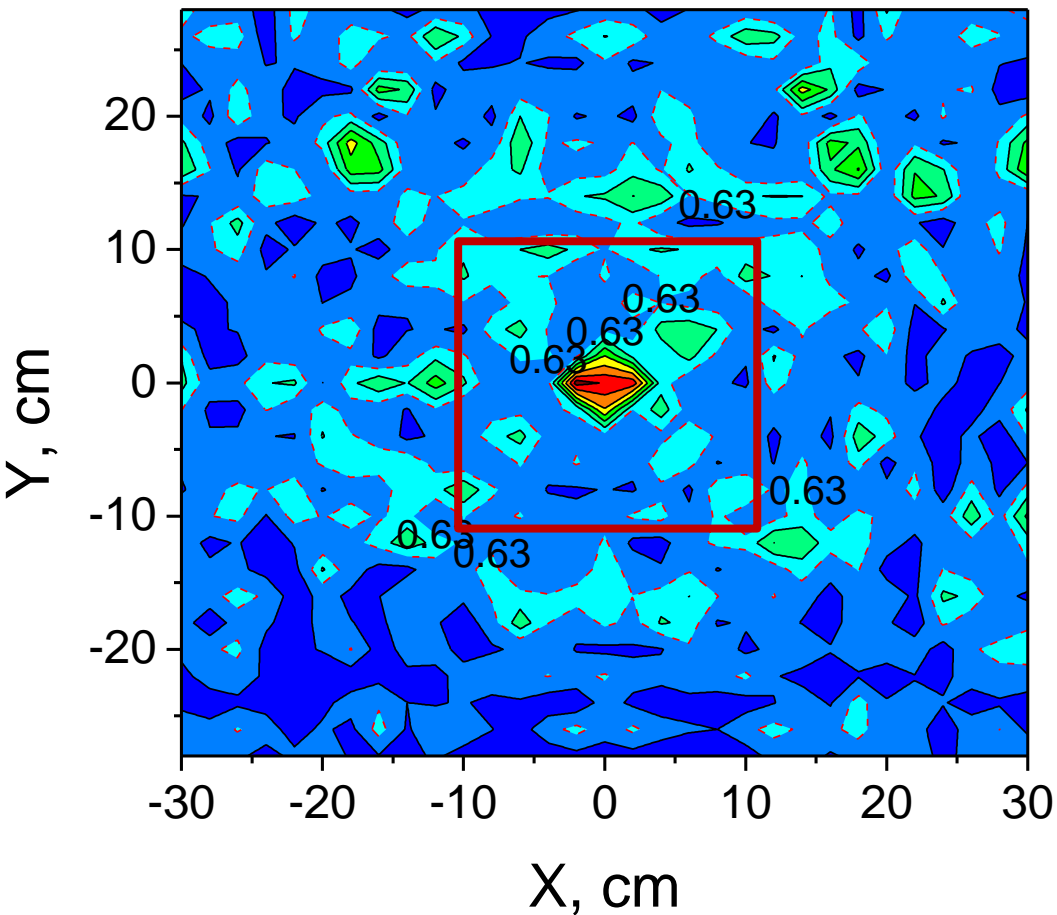
Acoustic Field Mapping (X-Y Plane, Z=+4cm)

- Cavitation threshold (0.63V)
- Effective scale (~10cm)



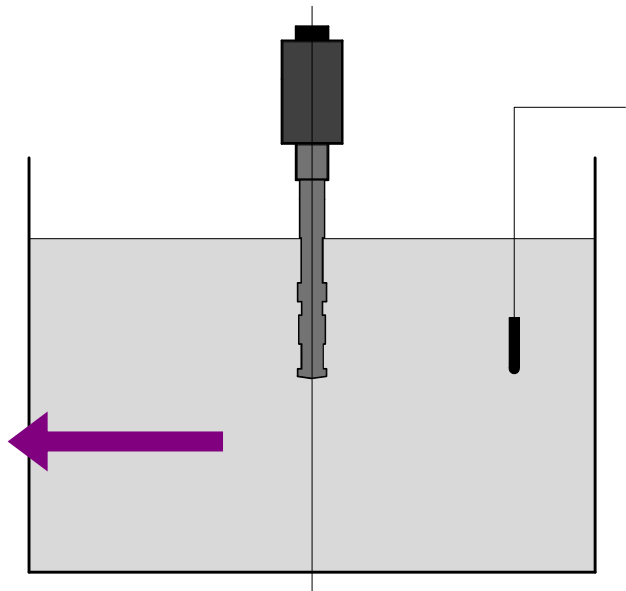
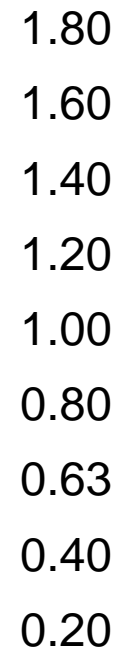
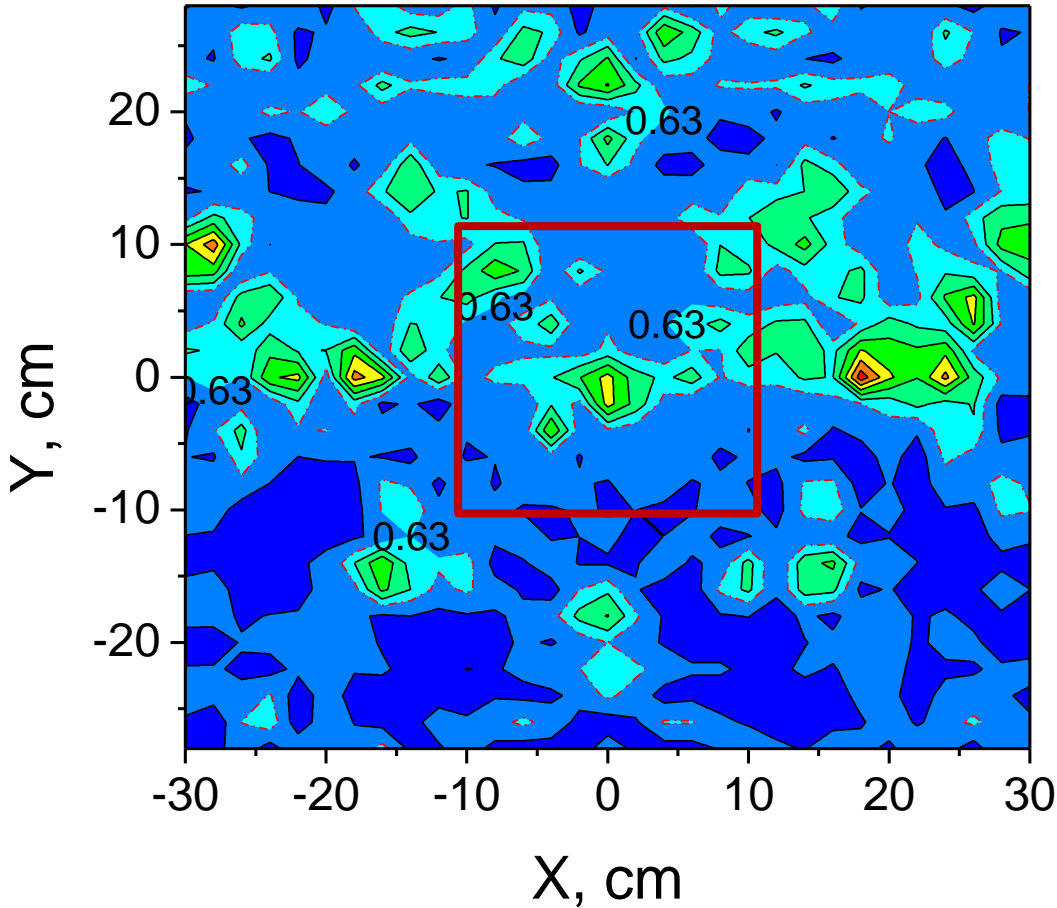
Acoustic Field Mapping (X-Y Plane, Z=0cm)

- Cavitation threshold (0.63V)
- Effective scale (<10cm)



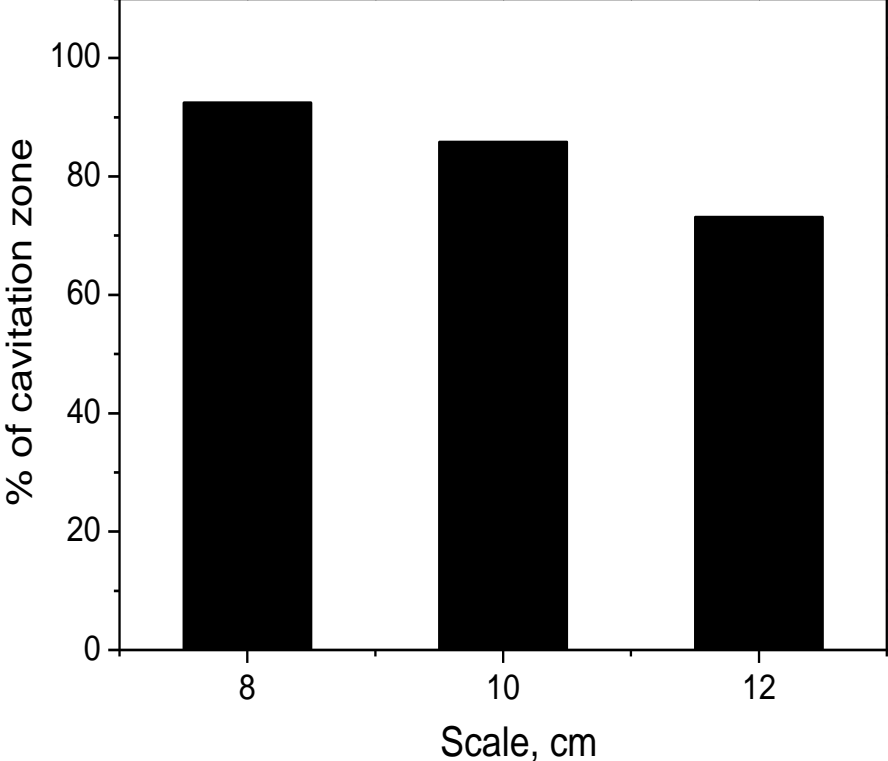
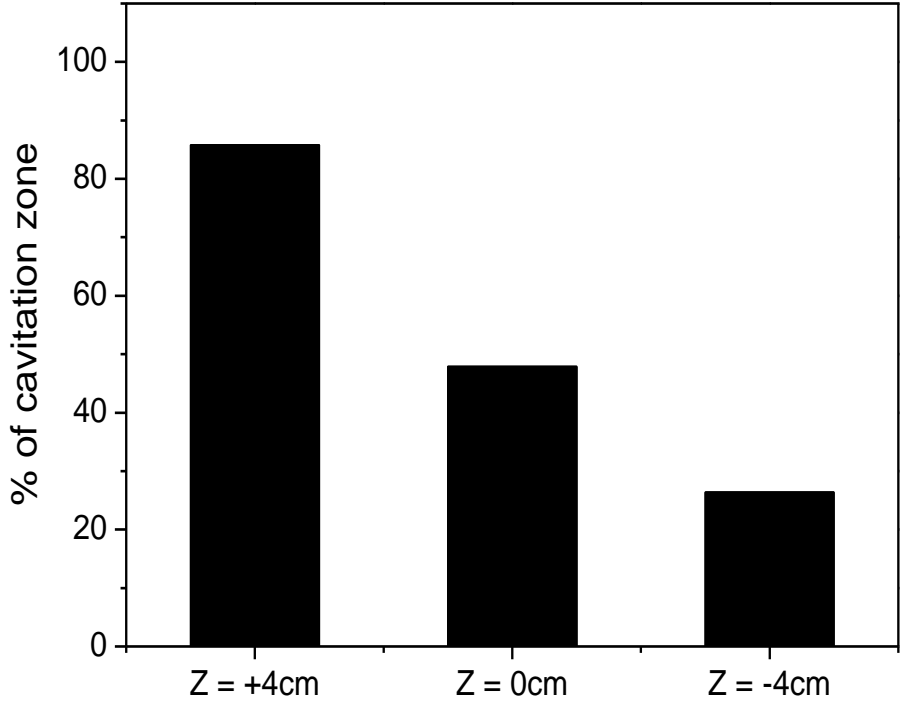
Acoustic Field Mapping (X-Y Plane, Z=-4cm)

- Cavitation threshold (0.63V)
- Effective scale (<10cm)



Percentage of Cavitation Zone in X-Y Plane

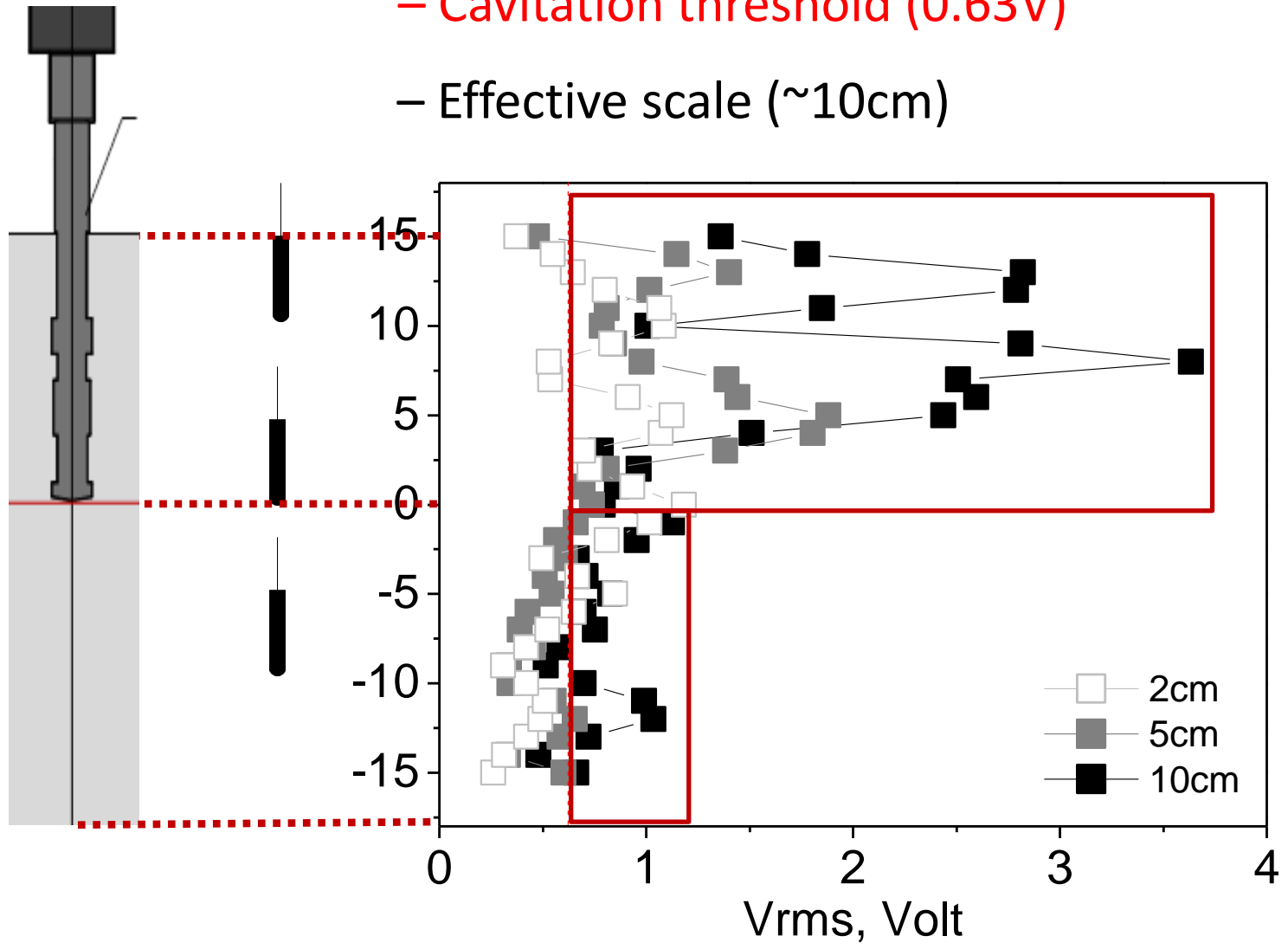
- Cavitation threshold (0.63V)
- Effective scale (~10cm)



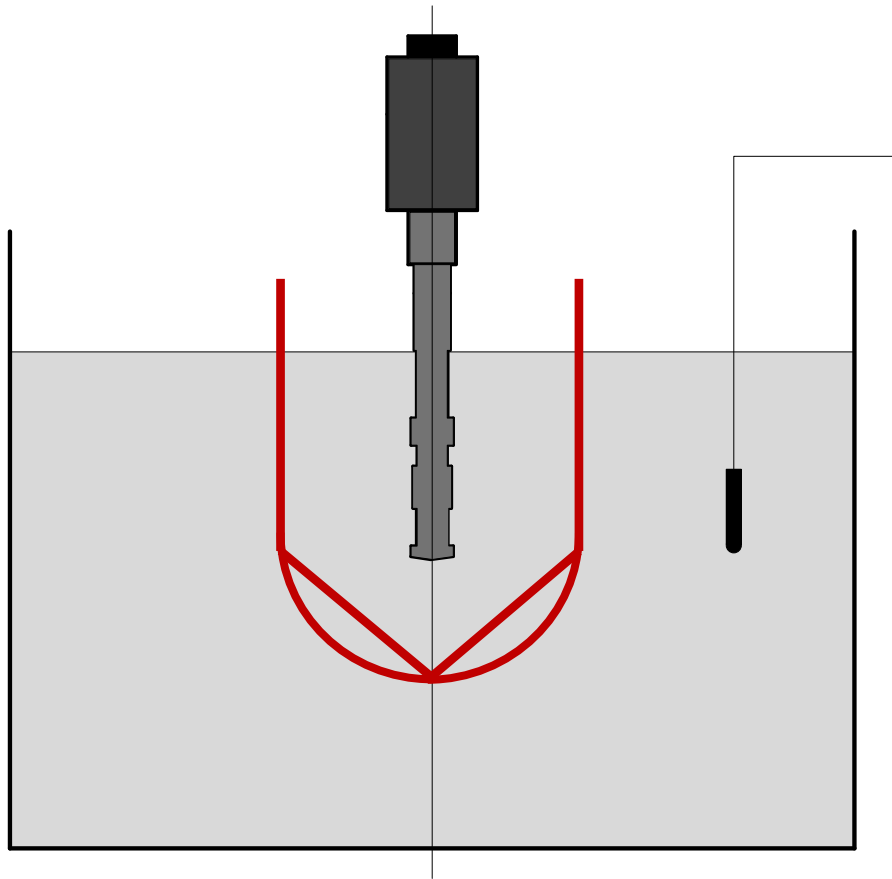
Acoustic Field Mapping (Z-Direction)

- Cavitation threshold (0.63V)

- Effective scale (~10cm)



Reactor Configuration



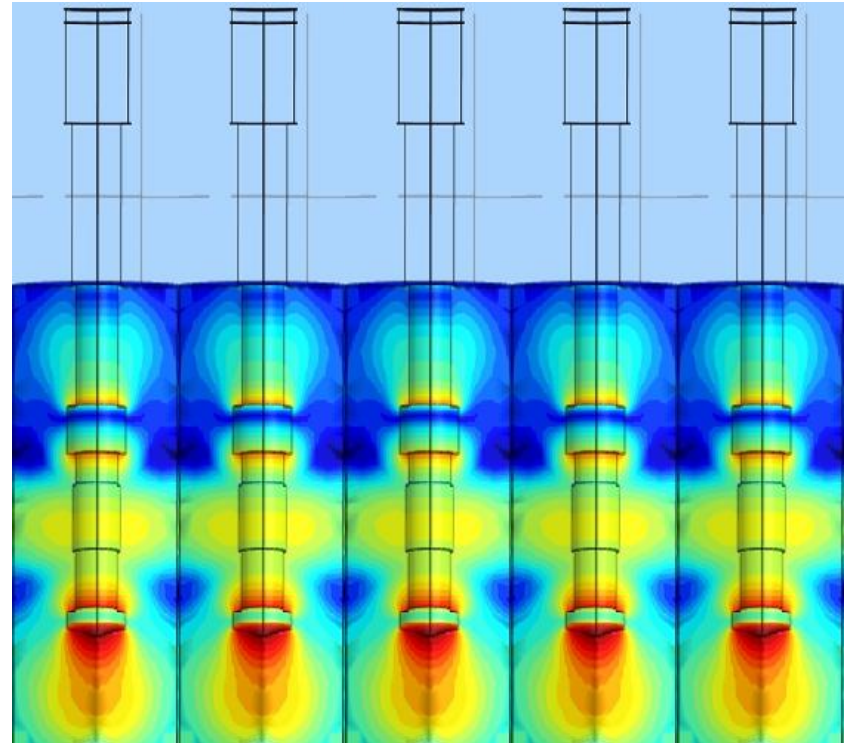
- Effective scale (10cm)
- Increase percentage of cavitation volume
- Treatment volume (~5.0L)



↑
50 mL

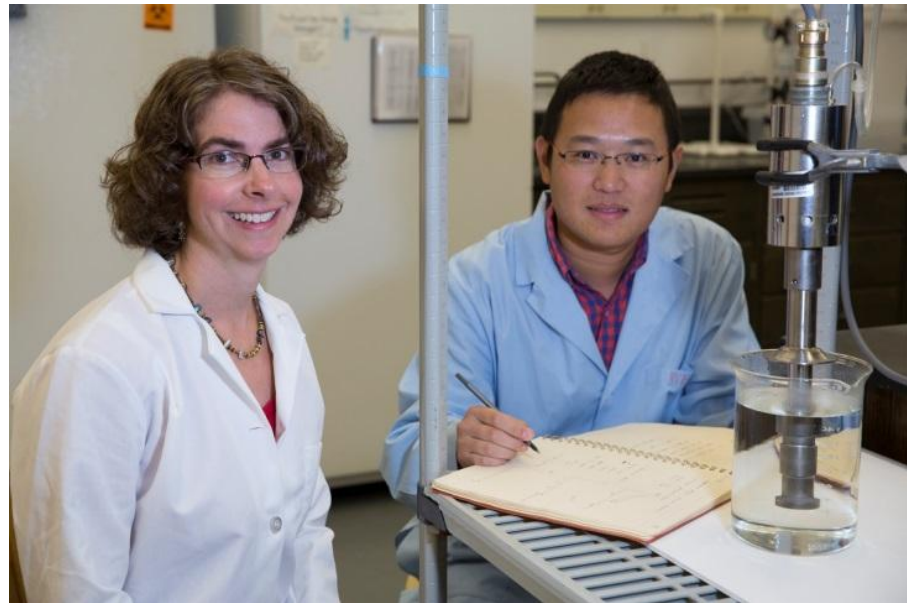
Summary and Future Work

- Multi-stepped shape – more energy-emitting surfaces
- Hydrophone – design large sono-reactors
- Large-volume reactor
- Array of designed horns
- Synergistic effect



Acknowledgement

- Dr. Linda Weavers
- James A Kosterman and ETREMA Products, Inc.
- Dr. Ruiyang Xiao, Dr. Meiqiang Cai, and Dr. Gim-Yang Pee

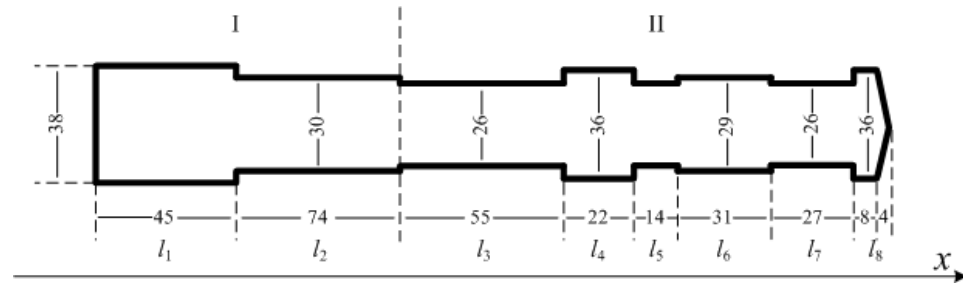
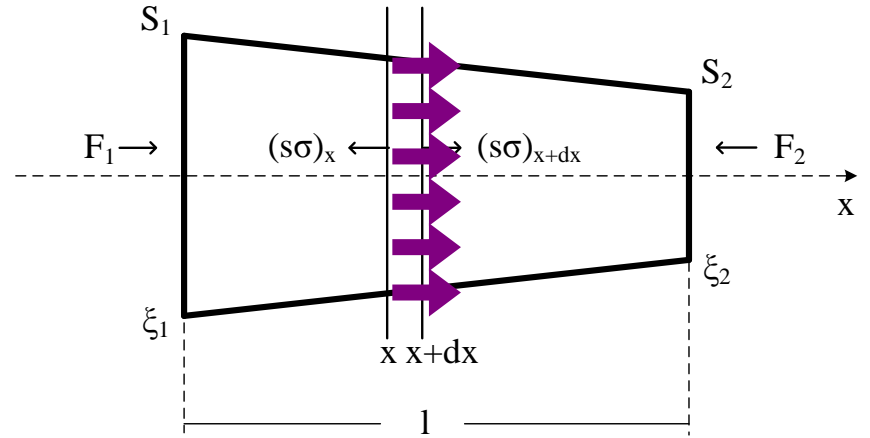


Thank You !

Backup Slides

Horn design requirements

- Resonance
 - *half-wave length*
 - $L = x \cdot (\lambda/2) = 280\text{mm}$
- Planar Homogeneous
 - $D < (\lambda/4) = 70\text{mm}$
- No concentrated energy
 - $Mp = 2.0$
- Multi-stepped shape
 - “edges”

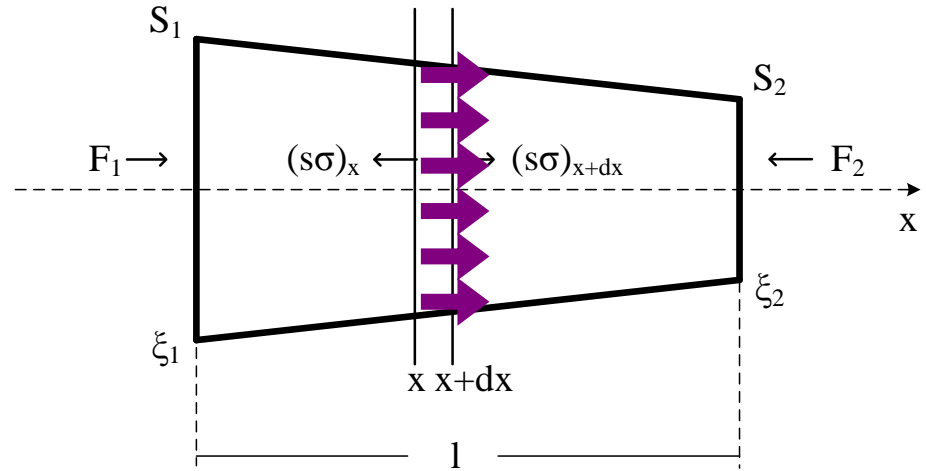


Design Principles

- Dynamic wave equation

$$\frac{\partial(S \cdot \sigma)}{\partial x} dx = S \cdot \rho \frac{\partial^2 \xi}{\partial t^2} dx$$

$$F = ma$$



- For a cylindrical horn in a steady-state mode

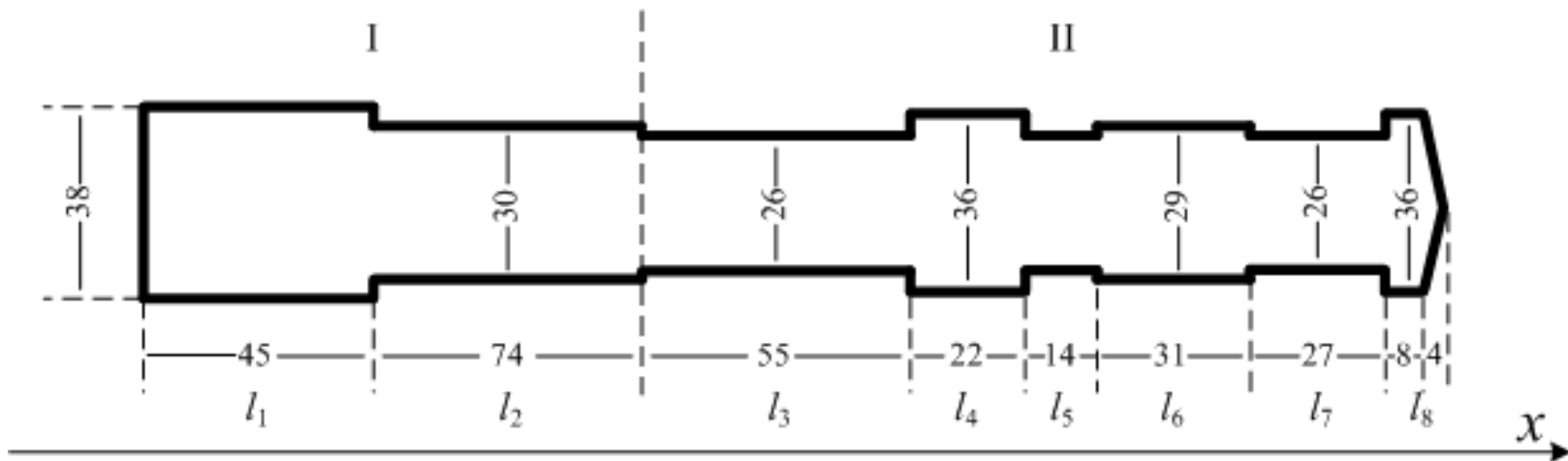
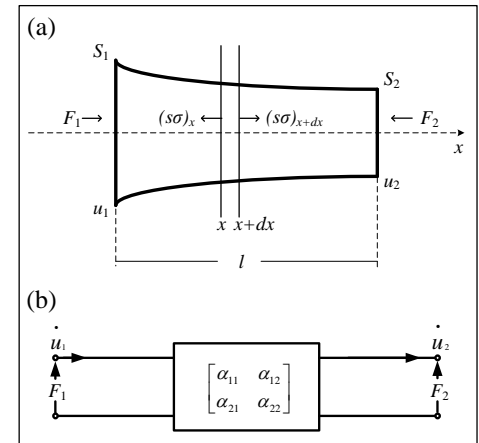
$$\frac{\partial^2 \xi}{\partial x^2} + k^2 \xi = 0$$

Design Principles

- Equivalent Circuit Model

$$\begin{bmatrix} \dot{u}_2 \\ F_2 \end{bmatrix} = \begin{bmatrix} \alpha_{11} & \alpha_{12} \\ \alpha_{21} & \alpha_{22} \end{bmatrix} \begin{bmatrix} \dot{u}_1 \\ F_1 \end{bmatrix}$$

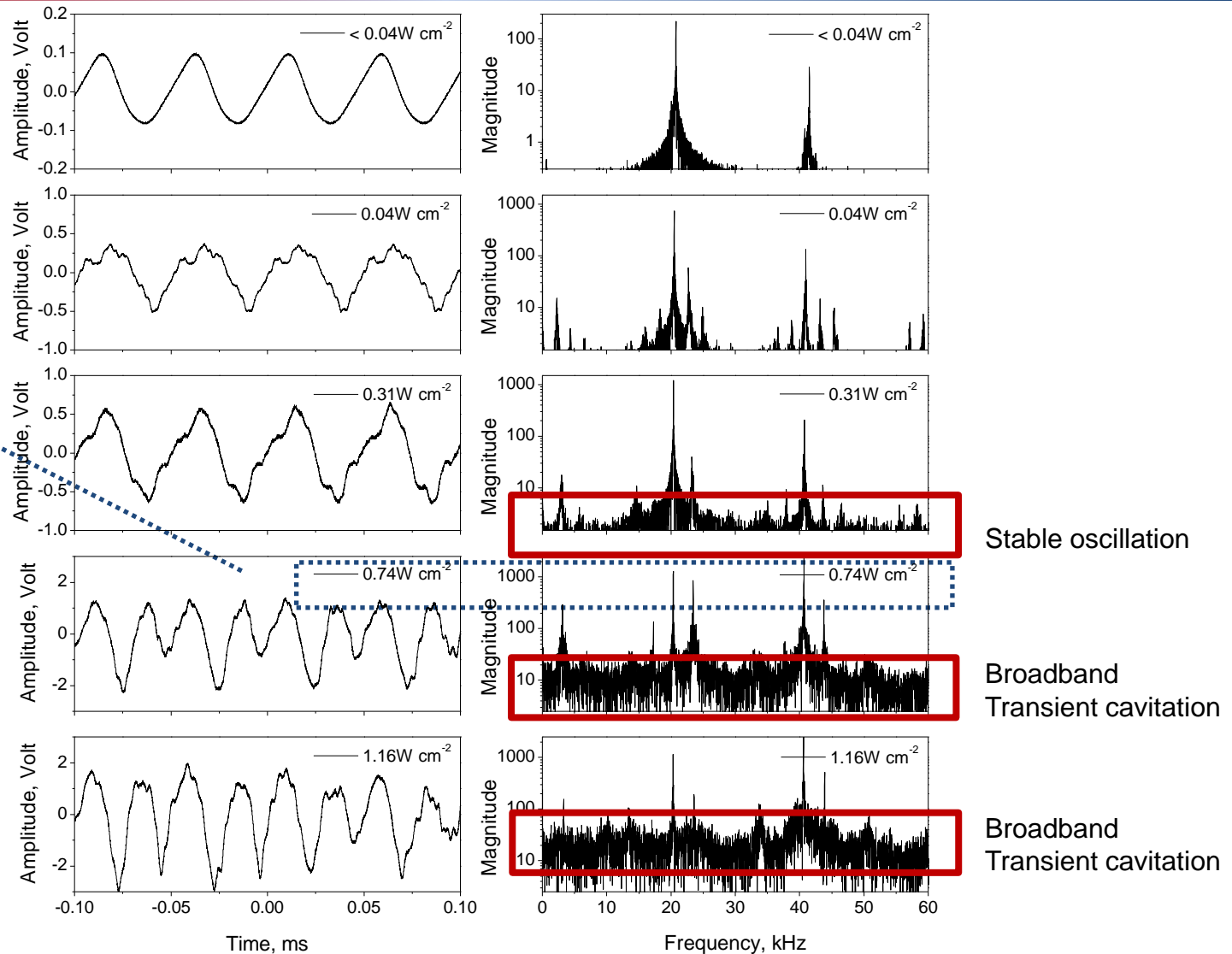
$$A = \begin{bmatrix} (\cos kl_8) & \frac{-j(\sin kl_8)}{\rho c Si} \\ -j\rho c Si(\sin kl_8) & (\cos kl_8) \end{bmatrix} \cdots \begin{bmatrix} (\cos kl_1) & \frac{-j(\sin kl_1)}{\rho c Si} \\ -j\rho c Si(\sin kl_1) & (\cos kl_1) \end{bmatrix}$$



Cavitation Threshold in Water

Threshold
for bubble
collapse!

0.63 Volt



Ultrasound waveforms and frequency spectrum observed from water at different power intensities

