

# Can power ultrasonic devices be printed?

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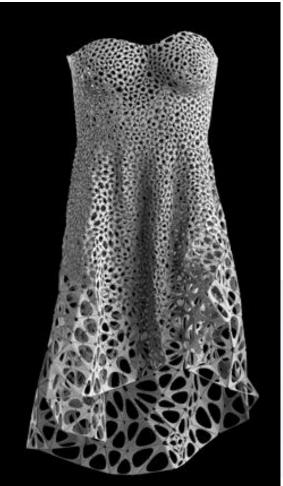


## Additive manufacture - Polymers / Ceramics





## Additive manufacture - Polymers / Ceramics











## Additive manufacture – Alloys







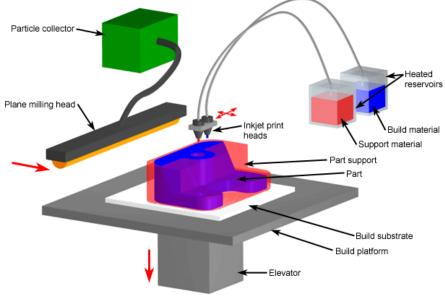




## Fundamentals: AM processes

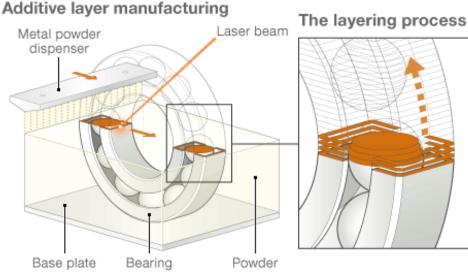
#### Extrusion deposition

#### Material is deposited direct on to substrate or previous layer



#### **Binding of granular materials**

Energy source is directed or a binder is applied to powder bed



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# Direct Metal Laser Sintering (DMLS)

#### Advantages (my opinion)

- Minimal material wastage
- Potential for highly complex shapes
- Short lead time: CAD model to manufactured part
- Fully machinable

#### Disadvantages (my opinion)

- Expensive
- Part surface required finishing
- Holes and threaded features required machined
- Cylindrical part not fully cylindrical

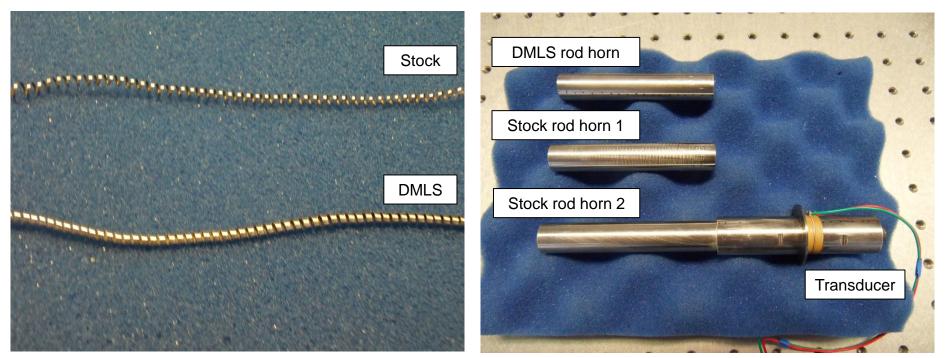


Optimisation of bracket



## Resonant parts

- Two rod horns machined from Ti6Al4V stock material
- One rod horn 'printed' via DMLS from Ti6Al4V powder



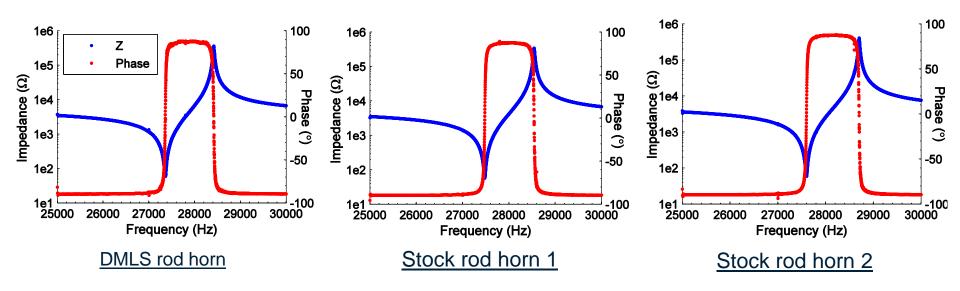
#### Titanium swarf

**Resonant device** 



## Impedance characteristics

#### Impedance traces





## Impedance characteristics

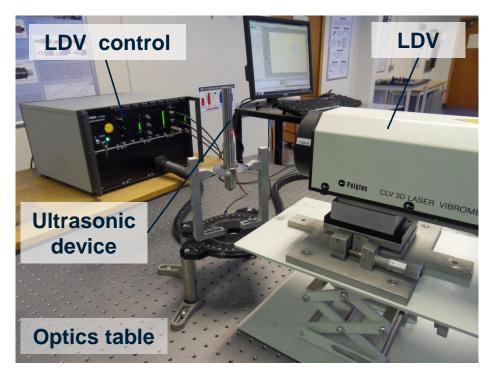
#### Impedance data

	DMLS rod horn	Stock rod horn 1	Stock rod horn 2
f <sub>s</sub>	27359Hz	27480Hz	27600Hz
f <sub>p</sub>	28416Hz	28544Hz	28705Hz
$Z_{fs}$	58Ω	57Ω	59Ω
k <sub>eff</sub>	0.2702	0.2705	0.2748
$Q_{m}$	977	981	986
	l		

	Average stock value	DMLS variation from average stock value	% diff (DMLS v average stock)
f <sub>s</sub>	27540Hz	-181Hz	0.66%
f <sub>p</sub>	28625Hz	-209Hz	0.73%
$Z_{fs}$	58Ω	ΟΩ	0.00%
k <sub>eff</sub>	0.2726	-0.0024	0.89%
$Q_m$	984	-6	0.66%



## Resonant frequency identification <u>Experimental modal analysis (EMA)</u>

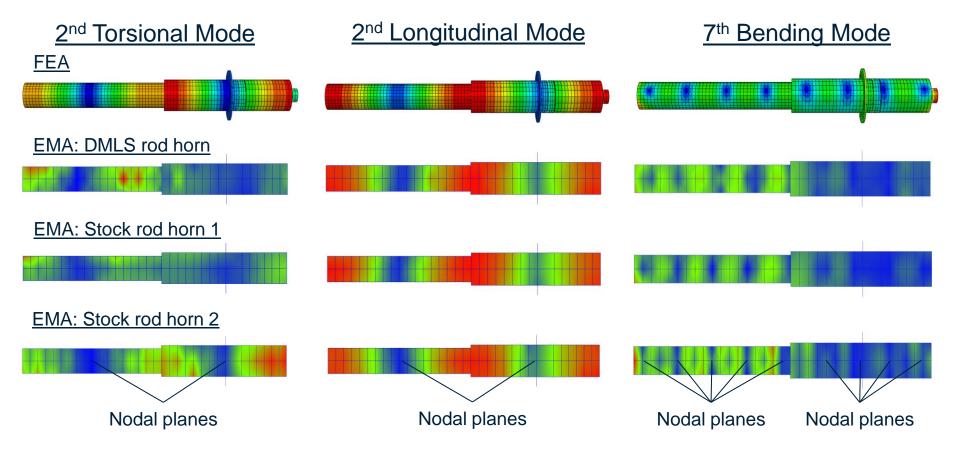


- Excitation frequency range 0-80 kHz
- Low power random excitation
- FRF resolution 1.6 Hz
- Experimental data undergoes curve fitting using ME'Scope software to generate a mathematical model of the transducer.



## Resonant frequency identification

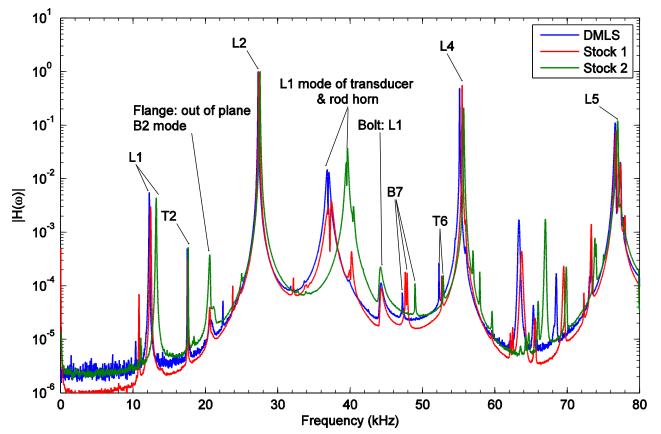
#### Modal analysis: Selected modes





## Resonant frequency identification

#### Modal Identification: FRFs with selected modes identified





## Resonant frequency identification

#### Modal Identification: Selected modes of vibration

	2 <sup>nd</sup> Torsional Mode f.		2 <sup>nd</sup> Longitudinal Mode f <sub>r</sub>		7 <sup>th</sup> Bending Mode f.	
FEA	18394Hz		28369Hz		50056Hz	
EMA	f <sub>r</sub>	% diff (FEA v EMA)	f <sub>r</sub> (Hz)	% diff (FEA v EMA)	f <sub>r</sub>	% diff (FEA v EMA)
DMLS Rod Horn	17492Hz	4.90%	27308Hz	3.74%	47231Hz	5.64%
Stock Rod Horn 1	17554Hz	4.56%	27416Hz	3.45%	47637Hz	4.83%
Stock Rod Horn 2	17638Hz	4.11%	27553Hz	2.88%	48986Hz	2.14%

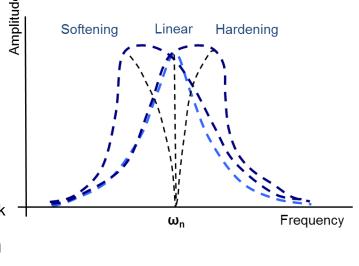


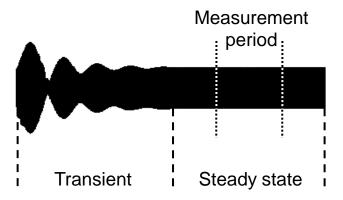
# Harmonic characterisation

Bidirectional frequency sweep technique

Sine burst

- Burst length: 4000 cycles
- At 27.5 kHz: burst length 0.14 seconds
- Devices excited at; 1,10, 20, 30, 40 and 50 V<sub>peak</sub>
- 1V<sub>peak</sub> excitation a 2 second time delay between successive bursts
- 10 50 V<sub>peak</sub> excitation level, a 10 second time delay between successive bursts

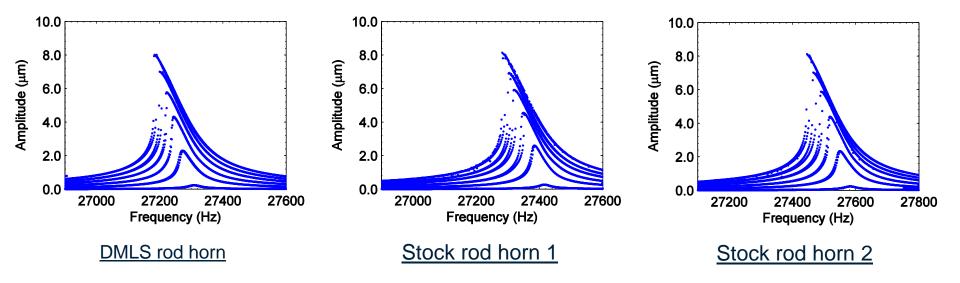






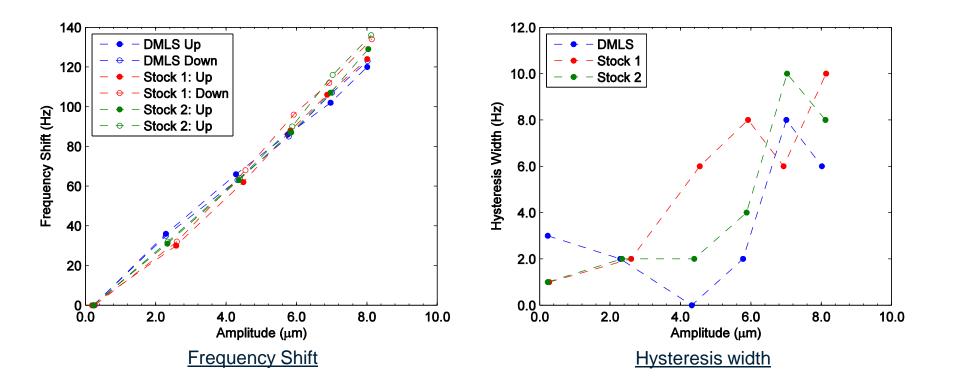
# Harmonic characterisation

**Bidirectional frequency sweep technique** 





## Harmonic characterisation





# Findings

- Yes.
- Limited differences between DMLS part and those manufactured from stock were observed.
- Great potential for novel designs to be incorporated into power ultrasonic devices.
- Further work is required to understand of how the grain / microstructure of DMLS alloys influences vibrational behaviour.



# Acknowledgements

Study funded by 2013-2014 Robertson Bequest Thanks to CeramTec UK Ltd for supplying PZT rings for the transducer

# Thanks for listening

**Questions?**